A Process Systems Framework for Design, Optimization and Control of Modular Energy Systems

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Presentation Outline



Introduction and Background

- Challenges and Opportunities for Natural Gas Utilization
- Process Intensification
- Process Systems Framework
- Process Operability Concepts

Proposed Approach

- Membrane Reactor Application
- Operability App for Design and Intensification

Strategies for High-D Modular Systems

- Parallel Computing and Natural Gas Combined Cycle Example
- Machine Learning (Gaussian Process) Mapping
- **Operability for Control and Estimation**
- Next Steps and Conclusions









http://www.eia.gov/pub/oil_gas/natural_gas/analysis_publications/ngpipeline/dependstates_map.html

After the shale gas revolution, according to the U.S. EIA,
 Appalachian region provided about 34% (2021) of the U.S. natural gas production*

 Specialized software tools that can assess technical and economic feasibility of natural gas utilization processes are needed

* Energy Information Administration, 2021





Methane Rich Gases Not Utilized



Flare Gas (\$100 million per month is burned at Bakken, ND)

Refinery Off Gas

Shale Gas

Coal-Bed Methane pum

- \checkmark These gases, which have been discovered but some remain untapped due to physical or economic reasons, are stranded
- \checkmark Effective utilization of these gases will have strong impact on science, economy, and environment





Conventional vs. Modular Natural Gas Utilization



- Explore distributed characteristics of feedstock (e.g., natural gas)
- ✓ Transport and/or assemble modular units or skids on site
- Need to address challenges associated with design and operation of modular plants



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Modular energy processes are operated in a *highly constrained* and integrated environment that is represented by complex *large-scale and nonlinear models*

There is an opportunity to employ process systems approaches to enable the design, intensification, and control of complex energy systems towards modularity





Process Intensification (PI)

Edited by Frerich J. Keil

WILEY-VCH

Modeling of Process Intensification





SECOND EDITION ENGINEERING FOR EFFICIENCY, SUSTAINABILITY AND FLEXIBILITY



Emerging equipment, ... promise spectacular improvements in process plants, markedly shrinking their size and dramatically boosting their efficiency*

PI is a strategy for making dramatic reductions in the size of a chemical plant so as to reach a given production objective**



*Stankiewicz & Moulijn, Chemical Engineering Progress, 2000 **Ranshaw, Proceedings -1st Intl. Conf. Proc. Intensif. for Chem. Ind., 1995

WestVirginiaUniversity.



Process Systems Framework







Operability Definition

Operability Analysis^{*,**}: Address operability challenges at the design phase



- Challenges:
- M^{-1} may not be straightforward to obtain
- High number of function evaluations (M and M^{-1})
- Operability approaches are usually tailored for specific applications

* Vinson D. R. and Georgakis C., *J. Process Control*, 2000 ** Gazzaneo V., Carrasco J.C., Vinson D. R., Lima F. V., *Ind. Eng. Chem. Res.*, 2020 West Virginia University

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Specific Objectives

- Extend operability concepts to address new directions on
 - ✓ design of high-dimensional nonlinear systems
 - ✓ process intensification towards modularity
 - dynamic operability for feasible modular operation under uncertainties
- Introduce bilevel optimization, parallel computing and machine learning-based approaches
- Apply developed approaches to modular system candidates
 - ✓ catalytic membrane reactor
 - ✓ natural gas combined cycle (NGCC)



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Modular Natural/Shale Gas System

Research Concept Catalytic Process Intensification for a Modular System



Direct Methane Aromatization Conversion in a Modular System

Catalytic Membrane Reactor Application



Endothermic reaction and Equilibrium controlled

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Membrane Reactor Model

<u>Molar balances:</u>

$$\frac{dF_{t,CH_4}}{dz} = r_1 A_t - \frac{Q}{\alpha_{H_2/CH_4}} \left(P_{t,CH_4}^{1/4} - P_{s,CH_4}^{1/4} \right) \pi d_t$$

$$\frac{dF_{t,C_2H_4}}{dz} = -\frac{r_1}{2} A_t + r_2 A_t - \frac{Q}{\alpha_{H_2/C_2H_4}} \left(P_{t,C_2H_4}^{1/4} - P_{s,C_2H_4}^{1/4} \right) \pi d_t$$

$$\frac{\frac{dF_{t,H_2}}{dz}}{dz} = -r_1 A_t - r_2 A_t - Q \left(P_{t,H_2}^{1/4} - P_{s,H_2}^{1/4} \right) \pi d_t$$

$$\frac{dF_{t,C_6H_6}}{dz} = -\frac{r_2}{3} A_t - \frac{Q}{\alpha_{H_2/C_6H_6}} \left(P_{t,C_6H_6}^{1/4} - P_{s,C_6H_6}^{1/4} \right) \pi d_t$$

Reaction mechanism **

Step 1:

$$r_{1} = k_{1} C_{CH_{4}} \left(1 - \frac{k_{1}' C_{C_{2}H_{4}} C_{H_{2}}^{2}}{k_{1} C_{CH_{4}}^{2}} \right)$$
Step 2:

$$r_{2} = k_{2} C_{C_{2}H_{4}} \left(1 - \frac{k_{2}' C_{C_{6}H_{6}} C_{H_{2}}^{3}}{k_{2} C_{C_{2}H_{4}}^{3}} \right)$$

 C_i : Concentration of species "*i*" r_1 and r_2 : reaction rates of steps 1 and 2 k_1 , k'_1 , k_2 , and k'_2 : reaction rate constants

*Iliuta et al. *Ind. Eng. Chem. Res.*, 2003 **Li et al., *Chem. Eng. Sci.*, 2002 West Virginia University.



First-principles model

Initial value problem, subroutine "ode15s"

experimental data*

Laboratory scale

(MATLAB)

 \geq

based on molar balances

Simulation validated with

- Input variables: L and d_t
 Outputs: CH₄ conversion, C₆H₆ production
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MR Operability Analysis



- High conversion does not translate to high benzene production
- The point "i" presents the best production of benzene
- Segment "g-h" shows the critical effect of length on production rate of benzene







MR Optimization-based Operability



- Reactor diameter (d_t) and length
 (L) show a large dispersion
- Design constraints: L <300 [cm] and L / d_t > 30* (for PFR)

*Rawlings, J. B. and Ekerdt, J. G. Chemical Reactor Analysis and Design Fundamentals; Nob Hill: Madison, WI, USA, 2002

Proposed framework is flexible as allows the computation of DIS from any DOS





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MR Process Intensification



- Desired level of performance can be specified
- Reduction of DMA-MR footprint (reactor volume and membrane surface area)
- When compared to base case point "e"
- MR design can be intensified by 77% volume reduction and 80% membrane area reduction
- Bilevel optimization problem may be formulated as tool for process intensification







Integrated Bilevel *Operability* Framework For Process Design and *Intensification*



Carrasco J.C. and Lima F.V. *AIChE Journal*, 2017 Carrasco J.C. and Lima F.V. *Comput. Chem. Eng.*, 2017

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NLP-based Method

Nonlinear programming (NLP)-based operability method

- Handles infeasible DOS with NLP-based model inversion
- Finds feasible spaces, feasible DOS (DOS*) and feasible Desired Input Set (DIS*)
- Feasible points can be used in other optimization layers
- Provides insights for changes in the selected AIS



Carrasco J. C. and Lima F.V., Comput. Chem. Eng., 2017



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Multimodel Operability Approach

<u>Multimodel operability representation</u>: Original nonlinear model paired polytopes $P_k = \{P_k^u, P_k^y\}$





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- Simplified representation
- Efficient quantification of operability regions
- Straightforward calculation of *M*⁻¹

Explore system modularization





Gazzaneo V., Lima. F.V., *Ind. Eng. Chem. Res.*, 2019 Gazzaneo V., Carrasco J.C., Vinson D. R., Lima F. V., *Ind. Eng. Chem. Res.*, 2020

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Process Operability App Project

Process Operability App*



https://fernandolima.faculty.wvu.edu/operability-app





*Gazzaneo V., Carrasco J.C., Vinson D. R., Lima F. V., Ind. Eng. Chem. Res., 2020



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DIS*



Process Operability App: Applications

Input-output mapping for selection of the DOS



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CODE

Process Operability App: Applications



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MR Bilevel Operability Analysis (4-D)

1000

900

800 700

600

500 400

300

200

100



Computational Time**

AOS calculations (Control Problem)

	System	Dointo	Time	
2		Points	[min:sec]	
	2x2	25	00:03	
	3x3	125	00:18	
	4x4	625	01:42	

DIS* calculations (Design Problem)

System	Points	Time	
System		[hr:min:sec]	
2x2	25	00:06:15	
3x3	125	01:25:02	
4x4	625	13:08:08	
Higher-D		???	
**Intel Ca			

Intel Core I/ (Sandy bridge) 3.40 GHz processor

Carrasco J.C. and Lima F.V. In Proceedings of the FOCAPO/CPC, 2017

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Operability Framework Based on Bilevel Optimization

Strategies Towards Computational Time Reduction

Parallel computing Machine learning (Gaussian Process) mapping



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Novel Operability Framework Based on Parallel Computing



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Carrasco J.C. and Lima F.V. AIChE Futures Issue, 2018





Computational Time Analysis for Parallelization





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CODES

Natural Gas Combined Cycle (NGCC) High-D Application – 8x8



* DOE/NETL-341/061013 Technical report, 2013

- Minimize size (power generation) of NGCC plant for intensification and modularity
- Maintain combined cycle efficiency

Capital Cost** [MM\$] = 2.821 (NPP)^{0.7991}

NPP: Net plant power [MW]

U.S. EIA, 2013. Updated capital cost estimates for utility scale electricity generating plants

ESMAP Technical paper 122/09. Study of equipment prices in the power sector

Carrasco J.C. and Lima F.V. AIChE Futures Issue, 2018



Selected intensified 5 inputs	Inputs points	
Natural gas feed [ton/h]	0.013	
HRSG steam feed [ton/h]	0.157	
Compressor outlet pressure [atm]	5.8	
Air feed temperature [K]	329	
Steam cycle pressure [atm]	140	

Selected intensified 5 outputs	Output points	
Net plant power [MW]	0.11	
Net plant efficiency [%]	56.5	
Capital cost* [\$ millions]	0.5	
Gas turbine power [MW]	0.09	
Air compressor power [MW]	0.06	

t.

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NGCC Computational Time Analysis

Subsystems	Points DOS	P3 Time [hr:min:sec]	P4 (63 cores) Time [hr:min:sec]	Reduction [times]
4x4	625	00:00:38	00:00:07	5.4
5x5	3125	00:05:06	00:00:19	16.1
7x7	78125	02:58:42	00:03:01	59.2
8x8	390625	16:56:26	00:14:24	70.6

NGCC plant computational time estimations:

- ✓ NGCC 10x10 system (63 cores) would require approx. 11,400 seconds
- ✓ If the NETL supercomputer (Joule*) was used:
 - ✤ 3 seconds would be estimated for 10x10 system
 - ✤ 3,600 seconds would be estimated for 22x22 system

*Joule is one of the top 100 supercomputers in the world, has 1512 nodes, each node has two 8core 2.6 GHz Intel Sandy Bridge CPUs, with approx. 17,000 available cores

Carrasco J.C. and Lima F.V. AIChE Futures Issue, 2018



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Machine Learning-based Operability

Proposed method: supervised machine learning to generate process model surrogates for the developed operability algorithms

Surrogate models should be able to:

- decrease computational time
- represent nonlinearities, input-output multiplicities, etc.
- be compatible with previous process operability algorithms (NLP-based and multimodel approaches)

Gaussian Processes: $\mathbb{GP} \stackrel{\text{def}}{=} \widehat{Y}(X) = \mu(X) + K(X)$



This concept has been extended to applications such as: Computer Experiments*, Flowsheet Optimization**, Real-time Optimization***



Extracted from https://towardsdatascience.com

* A. Forrester, A. Sobester and A. Keane, *John Wiley & Sons*, 2008; J. Sacks et al., *Statistical Science*, 1989 ** J. A. Caballero and I. E. Grossmann, *AIChE Journal*, 2008; *** M.V.C Gomes, PhD Thesis. *UFRJ*, 2007



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Machine Learning-based Operability



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Surrogate Model-based Operability Calculations

Case Study: Direct Methane Aromatization-Membrane Reactor (DMA-MR)



Alves V., Gazzaneo V. and Lima F. V., Submitted for Publication, 2021





Operability for Control and Estimation





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Dynamic Operability: DMA-MR Motivation



Challenges

- Intensified and modular units are harder to control due to the loss of degrees of freedom
- Under large disturbances, the process may not be able to return to the desired operating regions

Dynamic Operability Objective

- Construct the dynamically operable funnel: the operating region within which the process can always be retained regardless of the disturbances
- Dynamically operable funnel can be expressed as output constraints for MPC applications

Source: Gretarsson, Mahlzeit. "Marcellus Shale Revised Map 2019", Wikipedia, 23 Aug. 2019, https://en.wikipedia.org/wiki/File:Marcellus_shale_revised_map_2019.png.

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Dynamic Operability: Formulation

A dynamic process is operable if it can achieve desired performance requirements from the given inputs regardless of the realization of the disturbances

<u>Membrane reactor case study</u>: Disturbance is the methane concentration in the feed stream. If the dynamic disturbance only takes 2 values:

- Natural gas composition in the **first** well → First set of dynamic AOS (red)
- Natural gas composition in the second well → Second set of dynamic AOS (green)







Dynamic Operability: Results



If the **operable region exists** for every time step (from initial to invariant region time) **and** the **set points are inside** the final invariant regions, then the given steady-state design is **operable** ³⁴





Dynamic Operability Mapping



Dinh S. and Lima F.V. Accepted in PSE 2021+, 2022





Dynamic Operability Mapping Computation (Ongoing)



Dinh S. and Lima F.V. Accepted in PSE 2021+, 2022





Conclusions and Future Avenues

- Operability approaches provide new directions for process intensification of chemical and energy systems towards modularity
- Proposed bilevel optimization-based operability approaches using parallel computing and machine learning present themselves as alternatives to tackle computational time challenges
- Future avenues:
 - explore Gaussian Process methods for the dynamic mapping of operability
 - incorporate multiple objectives (e.g., economics, sustainability) into process operability
 - perform dynamic operability funnel updates using sensitivity calculations (with Larry Biegler)
 - ✓ develop operability open-source software in Python (with Carl Laird)
- Other research directions: <u>www.statler.wvu.edu/~fernando.lima</u> Contact: <u>Fernando.Lima@mail.wvu.edu</u>; <u>flima@andrew.cmu.edu</u>





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