

Surrogate Model based Optimal Synthesis of Solid Sorbent Carbon Capture Processes

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OUTLINE

- **Carbon capture processes**
- **Superstructure optimization**
- **Surrogate models for optimization**
- **MINLP formulation**
- **Case study**
- **Conclusions**

CO₂ CAPTURE PROCESSES

Most widely investigated capture technology: MEA solvent based postcombustion

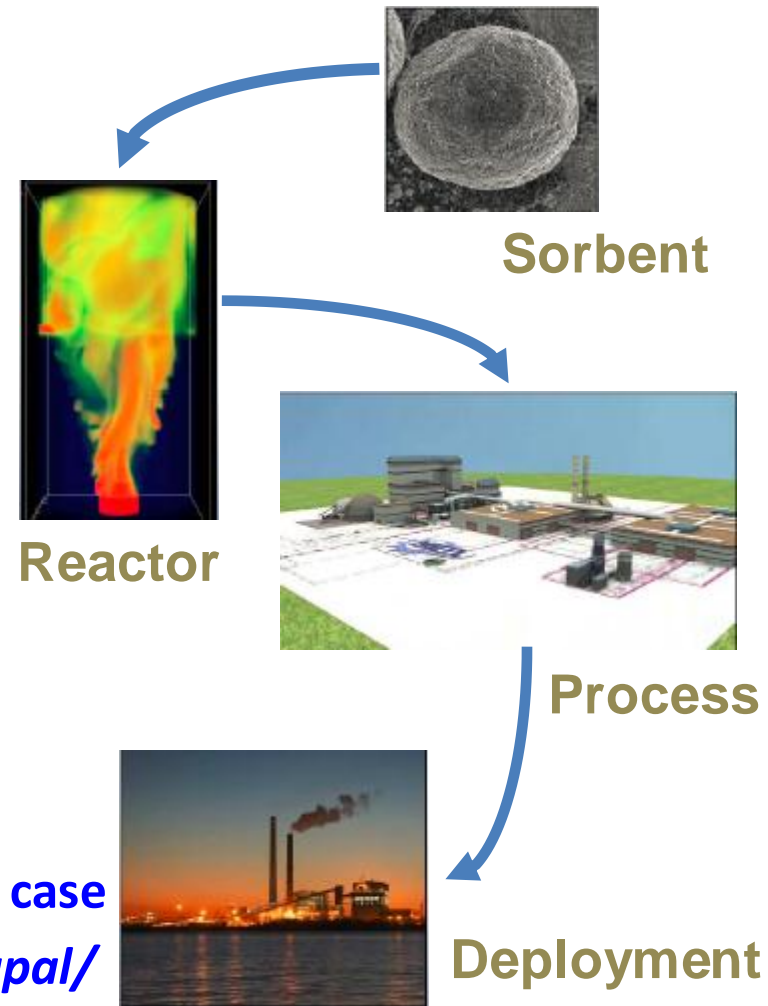
- Cost & energy-intensive technology
- Thermal & oxidative degradation

Innovative carbon capture technologies

- High-efficient solvents/sorbents
 - Greater capacity and selectivity
- Cost-effective capture process
 - Reduced energy for regeneration

DOE: Carbon Capture Simulation Initiative (CCSI)

- 5 National Labs and 6 Universities
- Solid sorbent technology: initial demonstration case
- <https://www.acceleratecarboncapture.org/drupal/>



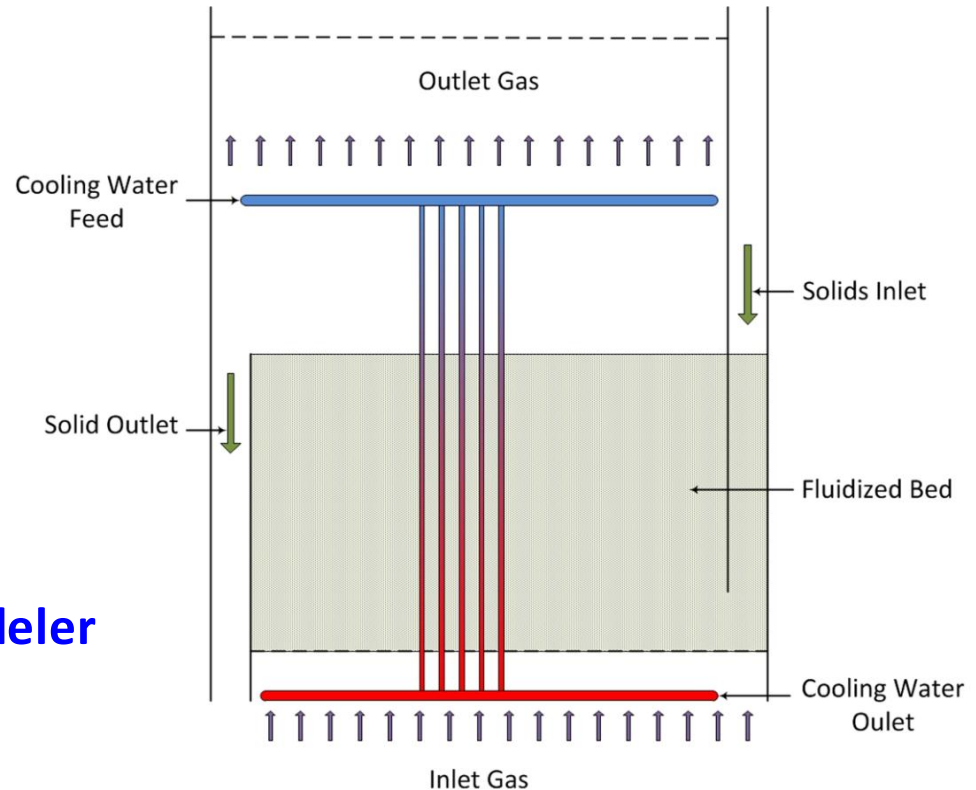
SOLID SORBENT CAPTURE PROCESS

Solid sorbent reactor

- *Bubbling fluidized bed*
- Fast fluidized bed
- Moving bed
- Fixed bed

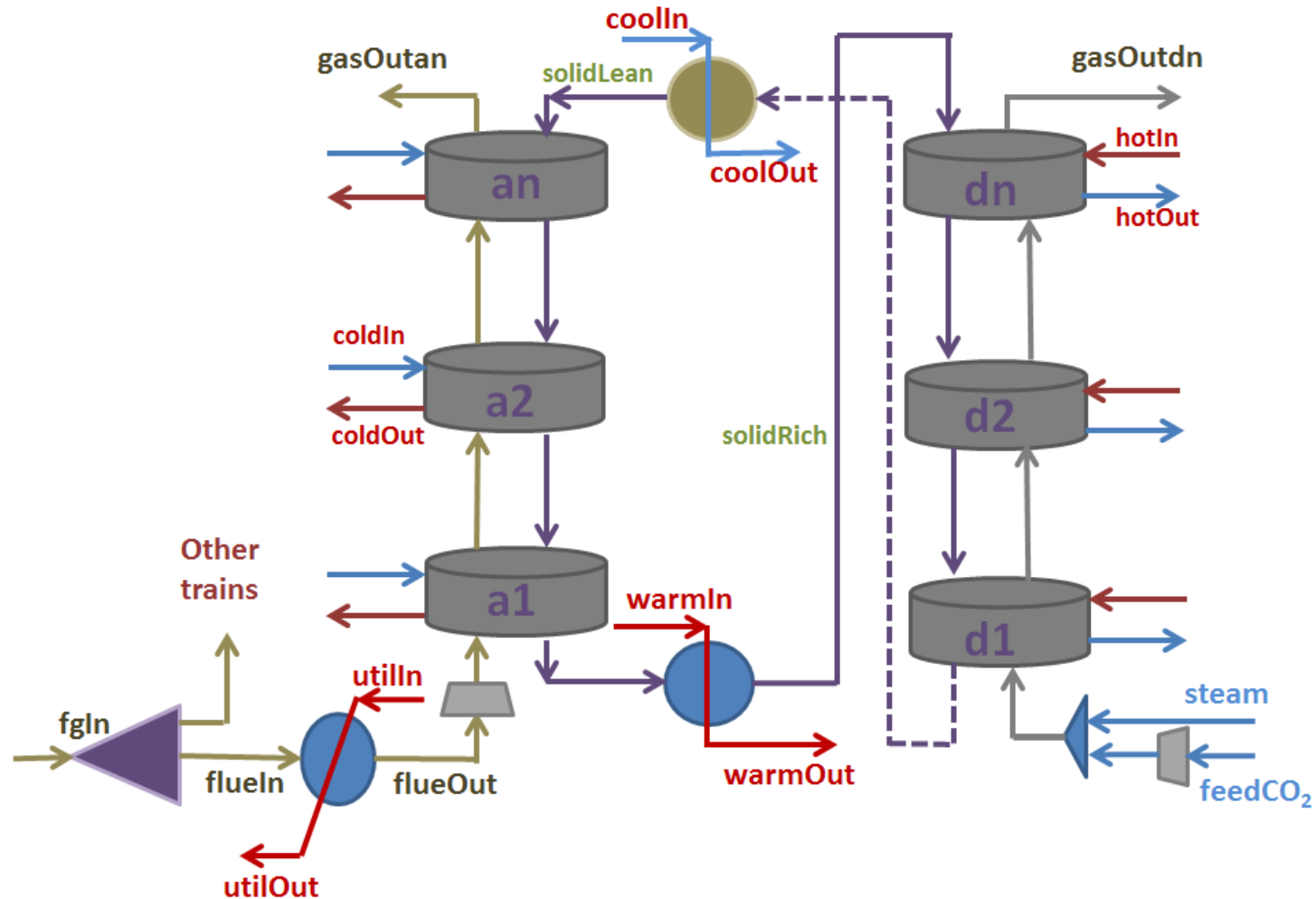
Bubbling fluidized bed

- 1D models
- Modeled in Aspen Custom Modeler
- Differential model
- Uses Aspen Properties package



(A Lee, D Miller. A one-dimensional(1-D) three-region model for a bubbling fluidized-bed adsorber. I&EC Research, 2013)

CO₂ CAPTURE PROCESS FLOWSHEET



General flow sheet for solid sorbent based carbon capture process

SUPERSTRUCTURE OPTIMIZATION

Objectives

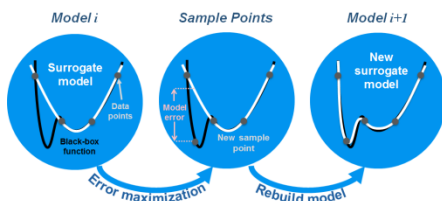
- Achieve the set carbon capture rate
- Minimize the cost of electricity (COE)
- Identify & develop the optimized bubbling fluidized bed process designs
 - Optimal topology
 - Optimal design conditions
 - Optimal operating conditions

Hurdles

- Computationally intractable because of the detailed first principle models

Handles

- Generate the set of low complexity algebraic surrogate models
 - Automated Learning of Algebraic Models for Optimization (ALAMO)



(<http://archimedes.cheme.cmu.edu/?q=alamo>)

SURROGATE MODEL GENERATION

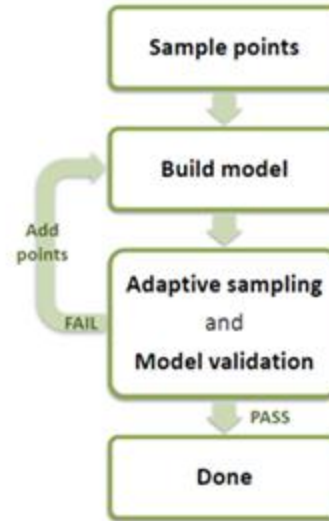
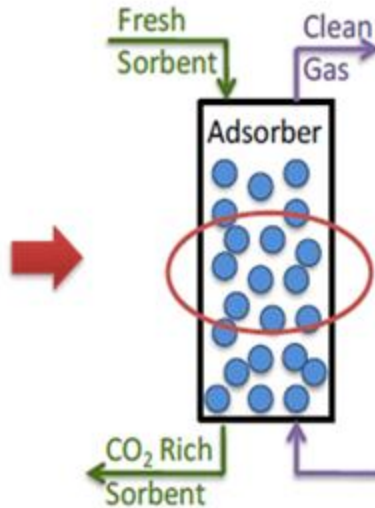
Process models

Aspen software

ALAMO

Surrogate models

$$x \in \mathbb{R}^D$$
$$x^l \leq x \leq x^u$$
$$\begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_d \\ \vdots \\ x_D \end{pmatrix}$$



$$\begin{pmatrix} z_1 \\ z_2 \\ \vdots \\ z_k \\ \vdots \\ z_K \end{pmatrix}$$
$$z \in \mathbb{R}^K$$
$$z = f(x)$$

Independent variables x

- Geometry
- Operating conditions
- Inlet flow conditions

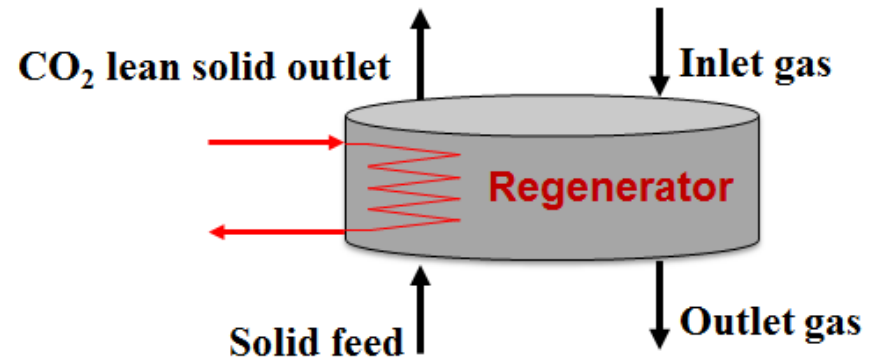
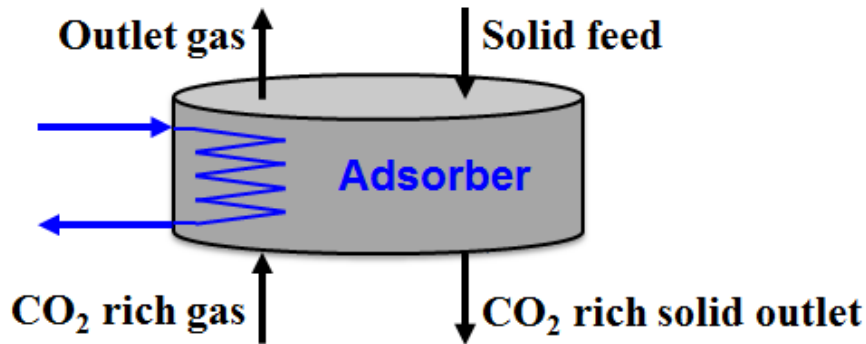
Dependent variables z

- Geometry required
- Operating condition required
- Outlet flow conditions
- Design constraints

(A. Cozad et al. Automatic learning of algebraic models for optimization. AIChE Journal, 2014)

BUBBLING FLUIDIZED BED

Bubbling fluidized bed reactor diagram



Model inputs

- Inlet pressure
- Inlet temperatures
- Inlet mass flow-rates
- Inlet gas mole fractions
- Inlet solid compositions
- Heat exchanger conditions

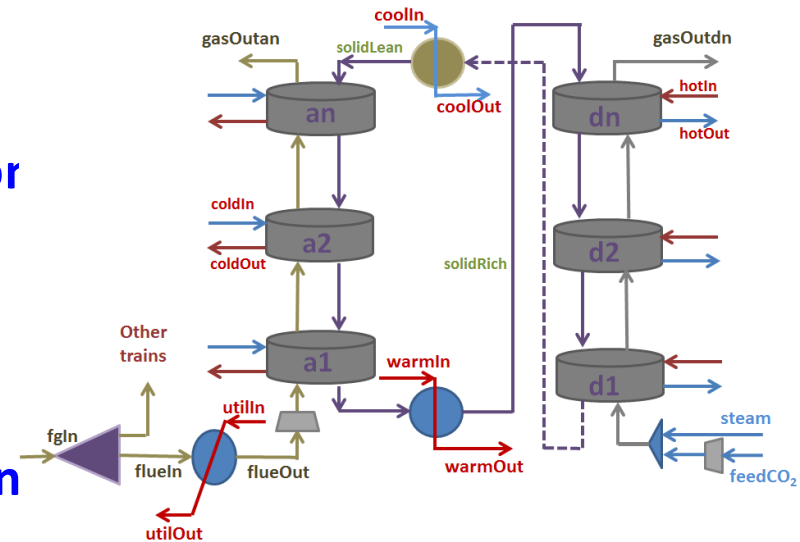
Model outputs

- Outlet pressure
- Outlet temperatures
- Outlet mass flow-rates
- Outlet gas mole fractions
- Outlet solid compositions

MINLP FORMULATION-ASSUMPTIONS

Assumptions for mixed integer nonlinear programming formulation

- Each stage is a single stage operation
- No pressure change for liquid and solid flow
- Each stage of adsorber/regenerator operation requires attached heat exchanger
- Surrogate models for fluidized bed adsorber and regenerator
- First principle models for SolidRich/SolidLean heat exchanger, blower, mixer



OBJECTIVE FUNCTION

Objective function

$$COE = \frac{(CCF)(TOC_{Sc} + TOC_{Cc}) + OC_{FIX} + (CF)(OC_{VAR})}{(CF)(MWh)} + COE_{TS\&M}$$

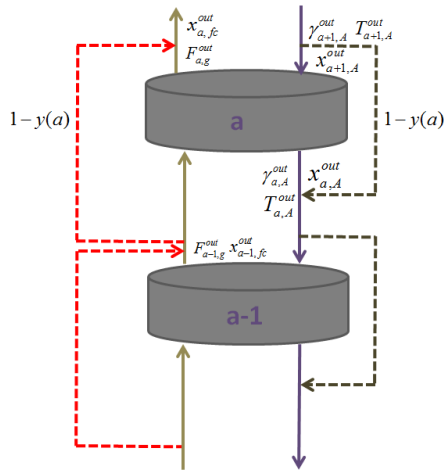
Where: $TOC_{Cc} = TOC_{Cs} + TOC_{rhx} + TOC_{lhx} + TOC_{flx}$

$$TOC_{Cs} = TOC_{ves} + TOC_{blow} + TOC_{HX} + TOC_{ele} + TOC_{pla} + TOC_{plat} + TOC_{elem}$$

- TOC_{Cc} : Capture system capital cost
- OC_{FIX} : Fixed operating & maintenance cost
- OC_{VAR} : Total variable cost
- MWh : Annual net megawatt-hours of power
- $COE_{TS\&M}$: COE increment
- TOC_{rhx} : Cost of Rich solid heat exchanger
- TOC_{lhx} : Cost of Lean solid heat exchanger
- TOC_{flx} : Cost of flue gas heat exchanger
- TOC_{Sc} : Sc plant capital cost
- TOC_{Cs} : Capital cost of reactors
- TOC_{ves} : Cost of vessel
- TOC_{blow} : Cost of blower
- TOC_{HX} : Cost of in-let heat exchanger
- TOC_{pla} : Cost of plate
- TOC_{plat} : Cost of platforms and ladders
- TOC_{elem} : Cost of elevator motor
- TOC_{ele} : Cost of elevator

MINLP FORMULATION

Adsorber series



- Flue gas flow**

$$x_{a,fc}^{out} = F(\text{surrogates})y(a) + x_{a-1,fc}^{out}(1-y(a))$$

$$F_{a,g}^{out} = F(\text{surrogates})y(a) + F_{a-1,g}^{out}(1-y(a))$$

$$T_{a,g}^{out} = F(\text{Surrogates})y(a) + T_{a-1,g}^{out}(1-y(a))$$

- Solid sorbent flow**

$$\gamma_{a,A}^{out} = F(\text{Surrogates})y(a) + \gamma_{a+1,A}^{out}(1-y(a))$$

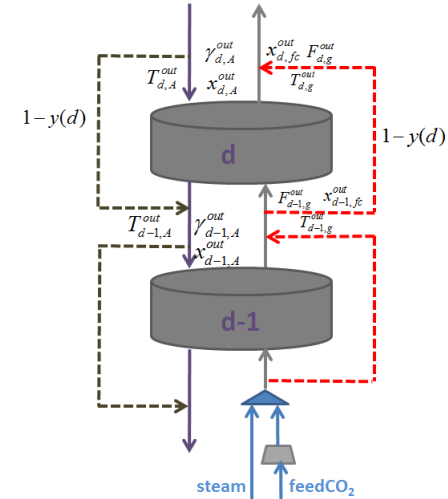
$$x_{a,A}^{out} = F(\text{Surrogates})y(a) + x_{a+1,A}^{out}(1-y(a))$$

$$T_{a,A}^{out} = F(\text{Surrogates})y(a) + T_{a+1,A}^{out}(1-y(a))$$

- Logical constraints**

$$y(s) \geq y(s+1), \forall s \in s_{\max} \quad \sum_s y(s) \geq 1 \quad \{a, d\} \in s$$

Regenerator series



- Clean gas flow**

$$x_{d,fc}^{out} = F(\text{surrogates})y(d) + x_{d-1,fc}^{out}(1-y(d))$$

$$F_{d,g}^{out} = F(\text{surrogates})y(d) + F_{d-1,g}^{out}(1-y(d))$$

$$T_{d,g}^{out} = F(\text{Surrogates})y(d) + T_{d-1,g}^{out}(1-y(d))$$

- Solid sorbent flow**

$$\gamma_{d,A}^{out} = F(\text{Surrogates})y(d) + \gamma_{d+1,A}^{out}(1-y(d))$$

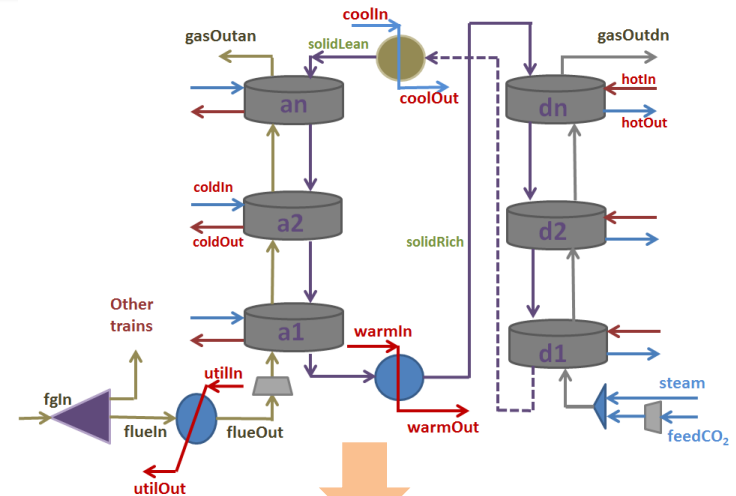
$$x_{d,A}^{out} = F(\text{Surrogates})y(d) + x_{d+1,A}^{out}(1-y(d))$$

$$T_{d,A}^{out} = F(\text{Surrogates})y(d) + T_{d+1,A}^{out}(1-y(d))$$

CASE STUDY

Given conditions

- Conditions of flue gas
- Max number of adsorbers: 4
- Max number of regenerators: 4
- Max number of trains: 16
- Minimum capture rate: 90%



Objectives

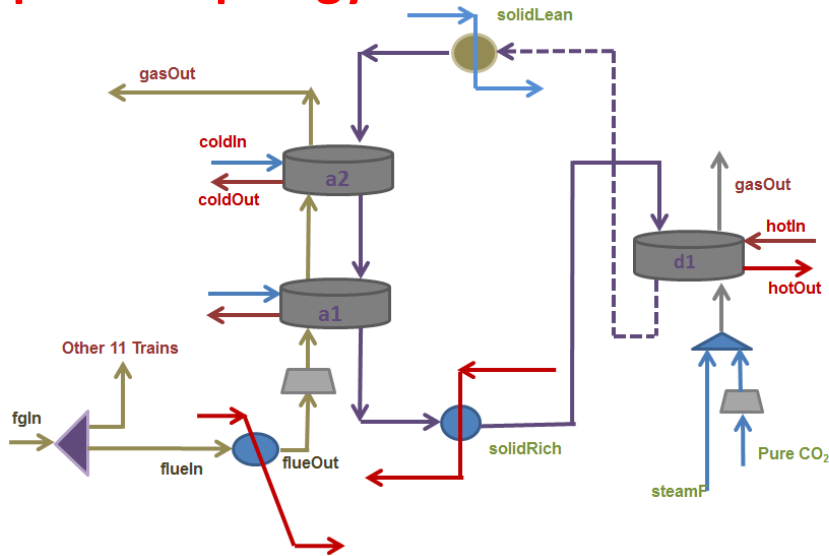
- Minimize cost of electricity
- Minimize total capital cost
- Decide the optimal number of trains in parallel
- Decide the optimal number of reactor in series
- Seek optimal operation conditions
- Seek an optimal geometry for each unit

Mixed-integer nonlinear programming model

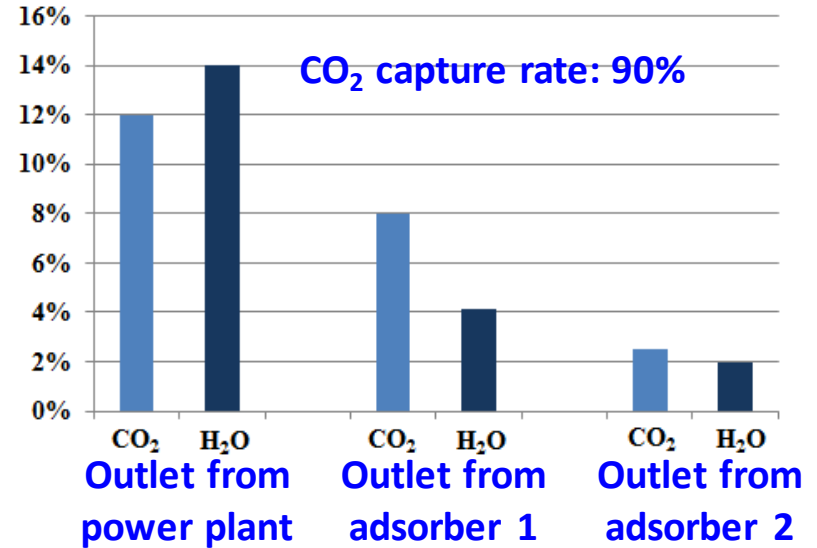
- Parameters
- Variables
- Equations
 - Economic modules
 - Process modules
 - Material balances
 - Hydrodynamic/Energy balances
 - Reactor surrogate models
 - Link between economic modules and process modules
 - Binary variable constraints
 - Bounds for variables

RESULTS

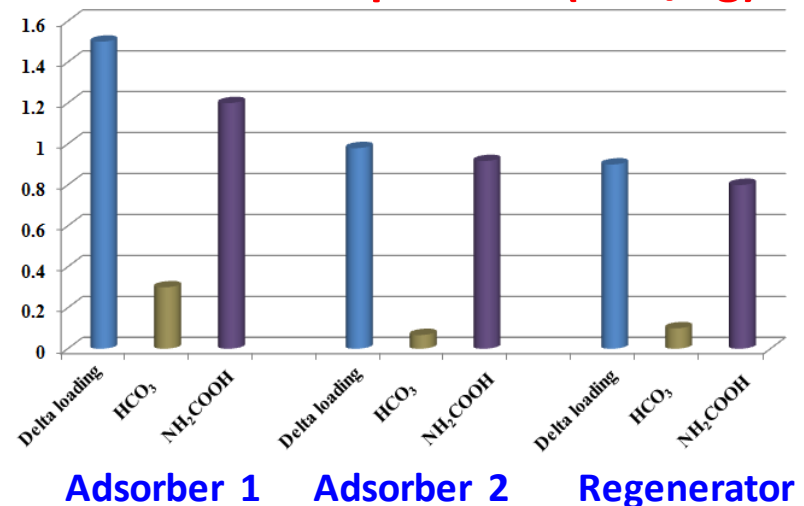
Optimal topology



Molar composition of flue gas



Outlet sorbent composition (mol/kg)



Variables	Lower	Value	Upper
COE(\$/MWh)*	0	137.3	1000
CapEX(\$M)	100	230.1	1000
steamFlow(kg/s)	~	108	~
Derate(MW)	0	103.7	650
sorbentF(kg/hr)	4E5	8.8E5	9E5
Nu (Number of trains)	12	12	16

* Cost of Electricity (COE) based on calculated capture system with base plant. + \$48/MWh to account for compression, transport & storage

CONCLUSIONS

- We developed a surrogate model based framework to seek the optimal topology and the relevant optimal design/operating levels for carbon capture processes
- ALAMO provides simple surrogate models of adsorbers and regenerators and thus leads to a low-complexity optimization model